

# DAE REDUX

Uri Ascher

Department of Computer Science  
UNIVERSITY OF BRITISH COLUMBIA

# OUTLINE

1. Numerical DAEs in the 1990's
2. Simulating deformable objects subject to friction and contact
3. Neural DAEs
4. Conclusions

DAE = Differential-Algebraic Equation

# NUMERICAL DAEs IN THE 1990's (SELECTIVE VIEW)

General form

$$\mathbf{F}(t, \mathbf{u}, \dot{\mathbf{u}}) = \mathbf{0}, \quad a \leq t \leq b$$

where  $\dot{\mathbf{u}} := \frac{d\mathbf{u}}{dt}$  and the Jacobian  $\frac{\partial \mathbf{F}}{\partial \dot{\mathbf{u}}}$  may be singular

Semi-explicit DAE  $\mathbf{u} = (\mathbf{x}, \mathbf{z})$

$$\dot{\mathbf{x}} = \mathbf{f}(t, \mathbf{x}, \mathbf{z}) \quad (1a)$$

$$\mathbf{0} = \mathbf{c}(t, \mathbf{x}, \mathbf{z}) \quad (1b)$$

- ▶ Can differentiate constraints (1b) repeatedly, until by plugging in (1a) can eliminate algebraic variables  $\mathbf{z}$  algebraically

Index = number of required differentiations + 1

[Brenan, Campbell & Petzold '95; Hairer & Wanner '96]

## EXAMPLE: EQUATIONS OF MOTION

- ▶ Masses times accelerations equal forces ( $\mathbf{v} = \dot{\mathbf{q}}$  in time  $t$ )

$$M\dot{\mathbf{v}}(t) = \mathbf{f}_{\text{els}}(\mathbf{q}) + \mathbf{f}_{\text{dmp}}(\mathbf{q}, \mathbf{v}) + \mathbf{f}_{\text{ext}} + \mathbf{f}_{\text{con}}$$

- ▶ with the elastic and damping forces

$$\mathbf{f}_{\text{els}}(\mathbf{q}) = -\frac{\partial}{\partial \mathbf{q}} W_{\text{els}}(\mathbf{q}), \quad \mathbf{f}_{\text{dmp}}(\mathbf{q}, \mathbf{v}) = -D\mathbf{v},$$

where  $W_{\text{els}}(\mathbf{q})$  is the elastic potential of the corresponding model

- ▶ Given position constraints

$$\mathbf{0} = \mathbf{c}(\mathbf{q})$$

we have constraint force  $\mathbf{f}_{\text{con}} = -G^T \mathbf{z}$  with  $G = \frac{\partial \mathbf{c}}{\partial \mathbf{q}}$  and  $\mathbf{z}$  Lagrange multiplier functions

- ▶ So to eliminate  $\mathbf{z}$  need to differentiate constraints twice: this is an **index-3 DAE**

# CONSTRAINT DRIFT-OFF

Continue with semi-explicit DAE

- ▶ By eliminating algebraic variables  $\mathbf{z}$  obtain a DE system with algebraic invariant
- ▶ However, simply ignoring the invariant manifold may lead to the numerical solution drifting off the constraints
- ▶ Various projection methods were proposed  
[Ascher & Petzold '98]
- ▶ Note also that for PDAEs constraint differentiation should be handled with extra care due to spatial boundary conditions  
[Sidilkover & Ascher '95]

# PENALTY METHODS

Continue with semi-explicit DAE

- ▶ Alternatively can use a **penalty approach** viewing the DAE as limit of a **singularly perturbed DE**

$$\varepsilon \dot{\mathbf{z}} = B\mathbf{c}(t, \mathbf{x}, \mathbf{z})$$

with parameter  $0 < \varepsilon \ll 1$  and matrix function  $B = B(\mathbf{u})$  carefully chosen

- ▶ However, the singularly perturbed DE can be more complex and demanding than the given DAE

# OUTLINE

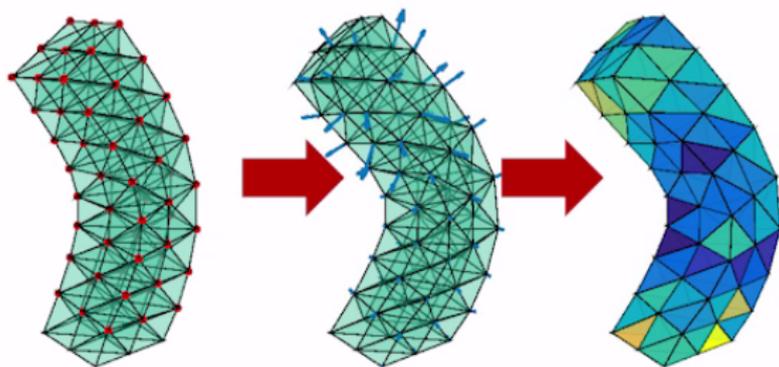
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[Larionov, Longva, Ascher, Bender & Pai '22; Larionov's PhD thesis '22]

# DEFORMABLE OBJECT SIMULATION

[Edwin Chen, Dinesh Pai; Danny Kaufman, Dave Levin;  
Bin Wang, Hui Huang]

- ▶ Ubiquitous in current computer graphics animation and robotics research
- ▶ High quality **simulations** can be very expensive to obtain
- ▶ For **control** and **fabrication** may require more accurate simulations



# DEFORMABLE OBJECT SIMULATION

For a given calibration (material properties):

- ▶ Semi-discretize **elastodynamics equations** in variational form using a **finite element method (FEM)** on a **moving tetrahedral mesh**
- ▶ Obtain a large ODE system (equations of motion) in time
- ▶ Define the **tangent stiffness matrix** at  $\mathbf{q} = \mathbf{q}(t)$  as
$$\mathbf{K} = -\frac{\partial}{\partial \mathbf{q}} \mathbf{f}_{\text{els}}(\mathbf{q})$$
- ▶ Write as  $\dot{\mathbf{u}}(t) = \mathbf{g}(\mathbf{u}(t))$

$$\begin{aligned} \dot{\mathbf{u}}(t) \equiv \begin{pmatrix} \dot{\mathbf{q}}(t) \\ \dot{\mathbf{v}}(t) \end{pmatrix} &= \begin{pmatrix} \mathbf{v} \\ M^{-1} \mathbf{f}_{\text{tot}}(\mathbf{q}, \mathbf{v}) \end{pmatrix} \\ &= \begin{pmatrix} 0 & I \\ -M^{-1} \mathbf{K} & -M^{-1} \mathbf{D} \end{pmatrix} \begin{pmatrix} \mathbf{q}(t) \\ \mathbf{v}(t) \end{pmatrix} + \begin{pmatrix} \mathbf{0} \\ \mathbf{r}(\mathbf{u}(t)) \end{pmatrix} \end{aligned}$$

Often there is **highly oscillatory stiffness** even though the observed motion is damped and is **not seen** to vibrate rapidly

# NONLINEAR FORCES

- ▶ Elastic forces: Neo-Hookean, StVK, Mooney-Rivlin, ARAP, artist-generated, etc.
- ▶ Often arise for large deformations  
[Ciarlet '88; Sifakis & Barbic '12]
- ▶ Stiffness matrix  $K$  depends on  $\mathbf{q}(t)$  and might become indefinite
- ▶ Damping forces: the popular Rayleigh force  
 $\mathbf{f}_{\text{dmp}}(\mathbf{q}, \mathbf{v}) = (a_0 M + a_1 K) \mathbf{v}$ , with parameters  $a_0, a_1 \geq 0$ , is good for theory
- ▶ Generally, modeling with nonlinear elastic forces as well as damping forces for visual purposes is still an open problem

## TIME DISCRETIZATIONS FOR $\dot{\mathbf{u}} = \mathbf{g}(\mathbf{u})$

At time  $t$  we know  $\mathbf{u}$  and seek  $\mathbf{u}_+$  at  $t_+ = t + h$

Can't use forward Euler or RK4 due to stiffness

- ▶ **Highly damping methods** e.g., BDF and Gauss-Radau  
Backward Euler (BE)

$$\mathbf{u}_+ = \mathbf{u} + h\mathbf{g}(\mathbf{u}_+)$$

- ▶ **Conservative methods** e.g., Trapezoidal (TR) and variants  
Implicit midpoint (IM)

$$\mathbf{u}_+ = \mathbf{u} + h\mathbf{g}((\mathbf{u}_+ + \mathbf{u})/2)$$

- ▶ **In-between methods**, still L-stable  
TR-BDF2

$$\mathbf{u}_* = \mathbf{u} + \frac{h}{4}(\mathbf{g}(\mathbf{u}_*) + \mathbf{g}(\mathbf{u}))$$

$$\mathbf{u}_+ = \mathbf{u}_* + \frac{1}{3}(\mathbf{u}_* - \mathbf{u} + h\mathbf{g}(\mathbf{u}_+))$$

# SEMI-IMPLICIT METHODS FOR $\dot{\mathbf{u}} = \mathbf{g}(\mathbf{u})$

Must solve nonlinear algebraic system for  $\mathbf{u}_+$  at each time step  $[t, t + h]$  — tough for **large** time steps  $h$

Fortunately, **absenting serious contact and friction effects** can often get away with semi-implicit versions

- ▶ **SI: semi-implicit BE**

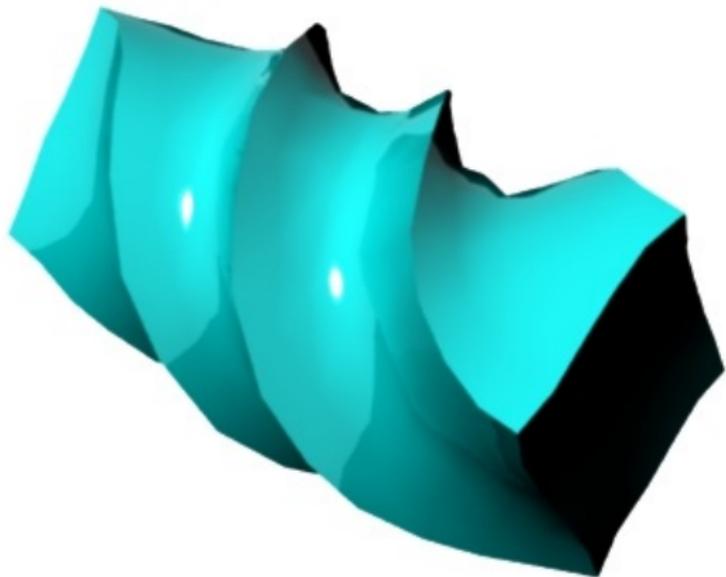
One iteration of Newton's method for BE step using **Jacobian** matrix  $J = \frac{\partial \mathbf{g}}{\partial \mathbf{u}}$

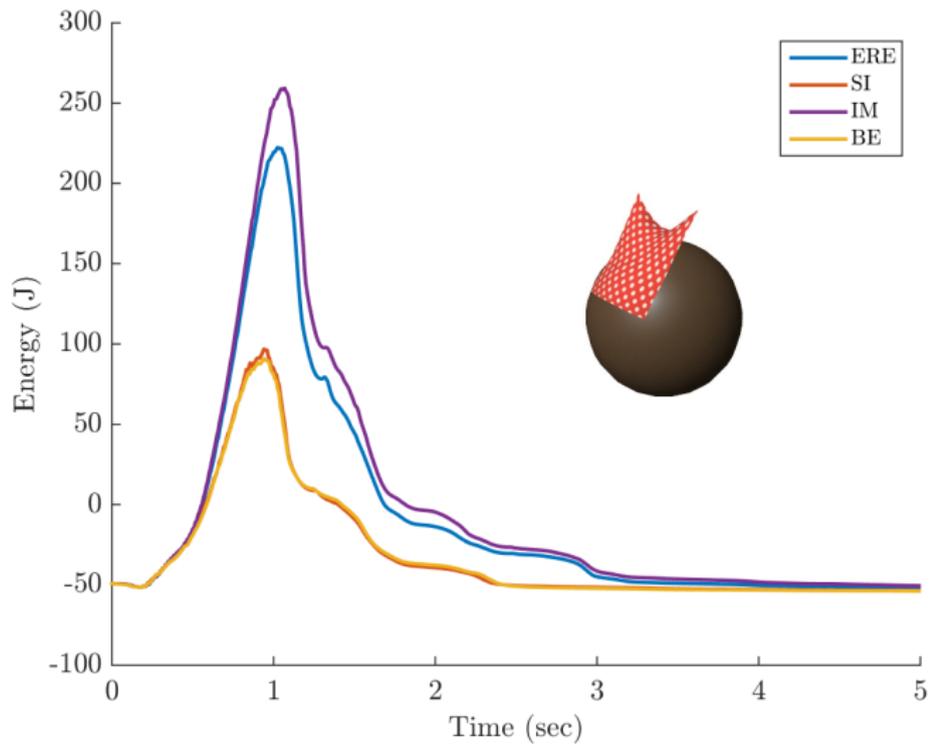
$$\mathbf{u}_+ = \mathbf{u} + h[\mathbf{I} - hJ(\mathbf{u})]^{-1}\mathbf{g}(\mathbf{u})$$

Solve a linear system of equations for  $\mathbf{u}_+$  at each time step

- ▶ **Exponential methods ERE and SIERE**

[Chen, Ascher & Pai '18; Chen, Sheen, Ascher & Pai '20]







# SIMPLE DAMPING ANALYSIS

[Chen, Ascher & Pai '18; Ascher, Larionov, Sheen & Pai '21]

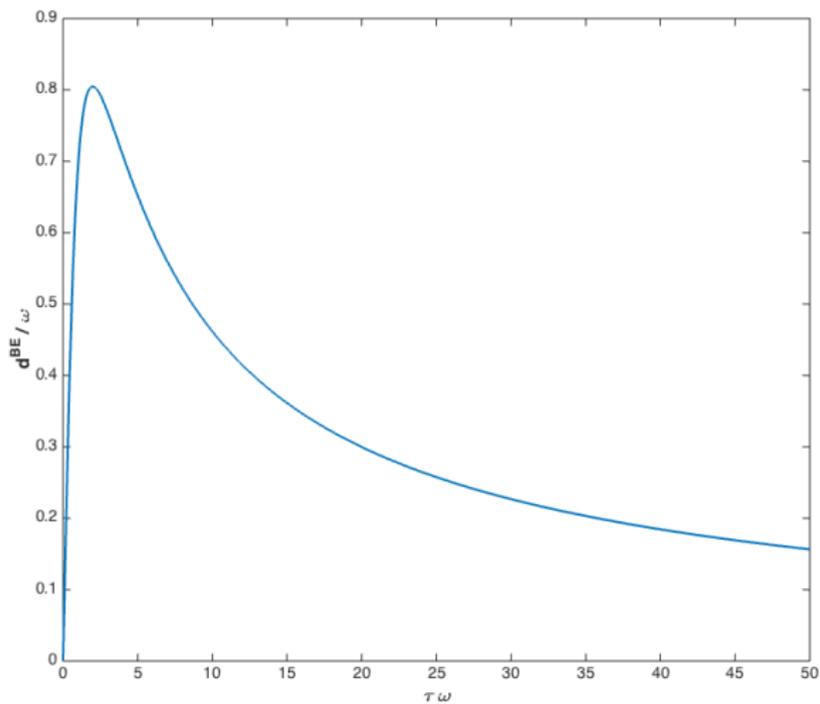
- ▶ Consider the scalar constant-coefficient ODE

$$\ddot{q} + d\dot{q} + \omega^2 q = 0$$

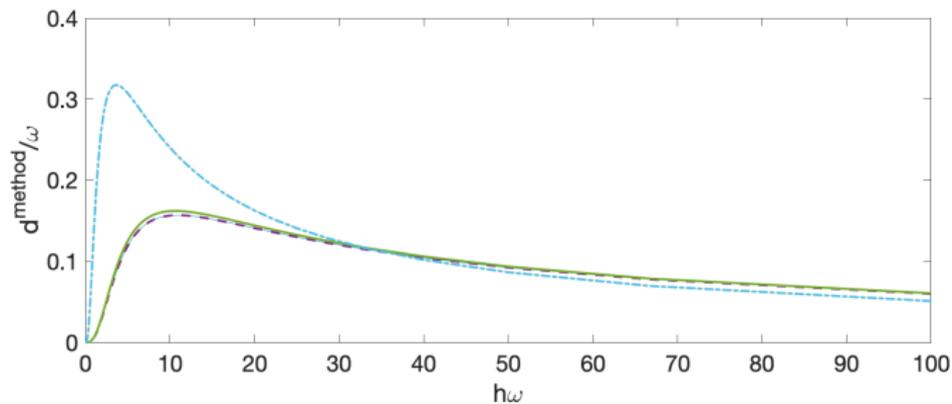
where  $d \geq 0$  is a **damping parameter**, and  $\omega > d/2$  is a real-valued **frequency**

- ▶ Setting  $d = 0$ , apply numerical discretization
- ▶ Associate resulting decay with artificial damping factor  $d^{\text{method}}$

# BE $\equiv$ SI ARTIFICIAL DAMPING CURVE

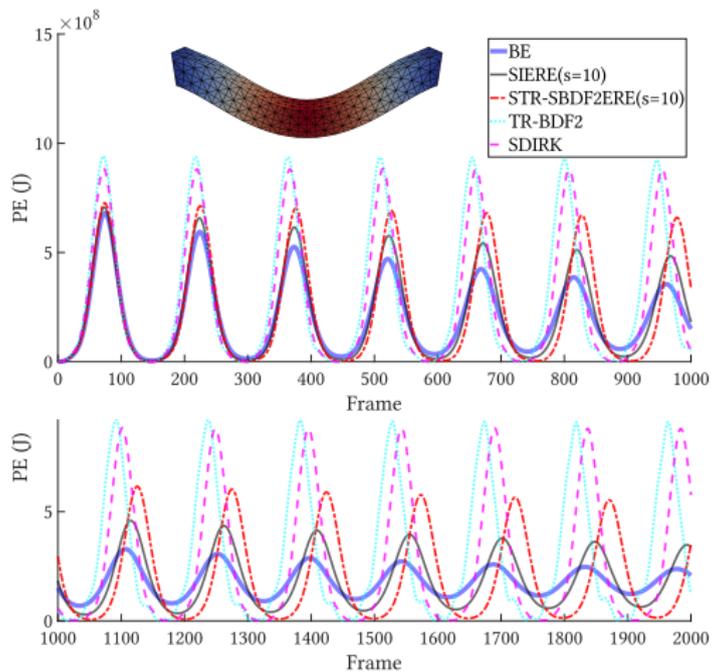


# BDF2 AND TR-BDF2 ARTIFICIAL DAMPING CURVES



Damping curves for TR-BDF2 (dashed) and BDF2 (dash-dot)

# COMPARING METHODS' ENERGIES



# ADDING CONTACT CONSTRAINTS

e.g. airplane landing, deformable objects colliding

- ▶ Must avoid mesh inter-penetration
- ▶ Handle inequality constraints that become equality upon contact
- ▶ Get **DAE** on subintervals with sensitive event locations, **DAI** otherwise
- ▶ In this setting **penalty** (and **interior point** + CCD) methods become attractive!
- ▶ Get a **differentiable model**

[Li, Ferguson, Langlois, Zorin, Panozzo, Jiang & Kaufmann '20]

[Geilinger, Hahn, Zehnder, Bacher, Thomaszewski & Coros '20]

# CONTACT CONSTRAINT FORCE

- ▶ Penalty function

$$b(x; \delta, \kappa) = \kappa \begin{cases} -(x - \delta)^3 & x < \delta \\ 0 & \text{otherwise} \end{cases}$$

- ▶ Apply to each contact point  $d_i = d_i(\mathbf{q})$  giving contact energy

$$W_{\text{con}}(\mathbf{q}) = \sum_i b(d_i; \delta, \kappa)$$

- ▶ Obtain contact force

$$\mathbf{f}_{\text{con}} = -\frac{\partial W_{\text{con}}}{\partial \mathbf{q}}$$

## TIME-STEPPING VIA “OPTIMIZATION”

For constrained deformable objects must at each time step solve nonlinear algebraic system carefully

- ▶ Consider e.g. BE for elastic plus contact forces

$$\begin{aligned} M(\mathbf{v}_+ - \mathbf{v}) &= h\mathbf{f}(\mathbf{q}_+, \mathbf{v}_+) = h(\mathbf{f}_{\text{els}}(\mathbf{q}_+) + \mathbf{f}_{\text{con}}(\mathbf{q}_+)) \\ &= -h \left( \frac{\partial W_{\text{els}}}{\partial \mathbf{q}} + \frac{\partial W_{\text{con}}}{\partial \mathbf{q}} \right) \end{aligned}$$

- ▶ So  $\mathbf{v}_+$  solves the optimization problem

$$\min_{\mathbf{v}_+} \frac{1}{2} \|\mathbf{v}_+ - \mathbf{v}\|_M^2 + h(W_{\text{els}}(\mathbf{q}_+) + W_{\text{con}}(\mathbf{q}_+))$$

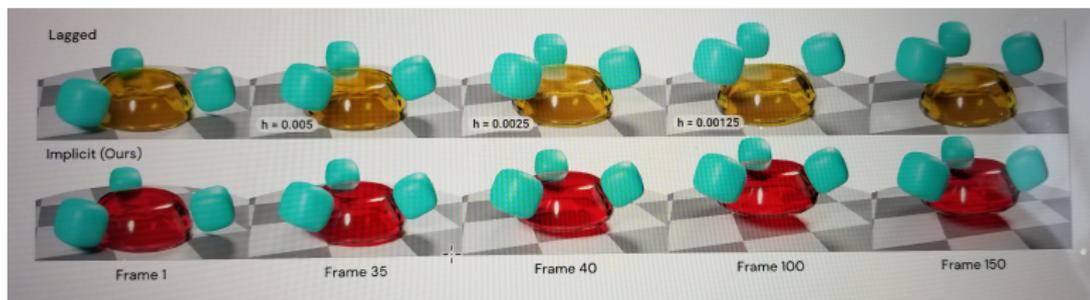
where  $\mathbf{q}_+ = \mathbf{q} + h\mathbf{v}_+$

- ▶ Potentially neater than solving the nonlinear equations using more general controlled damped Newton

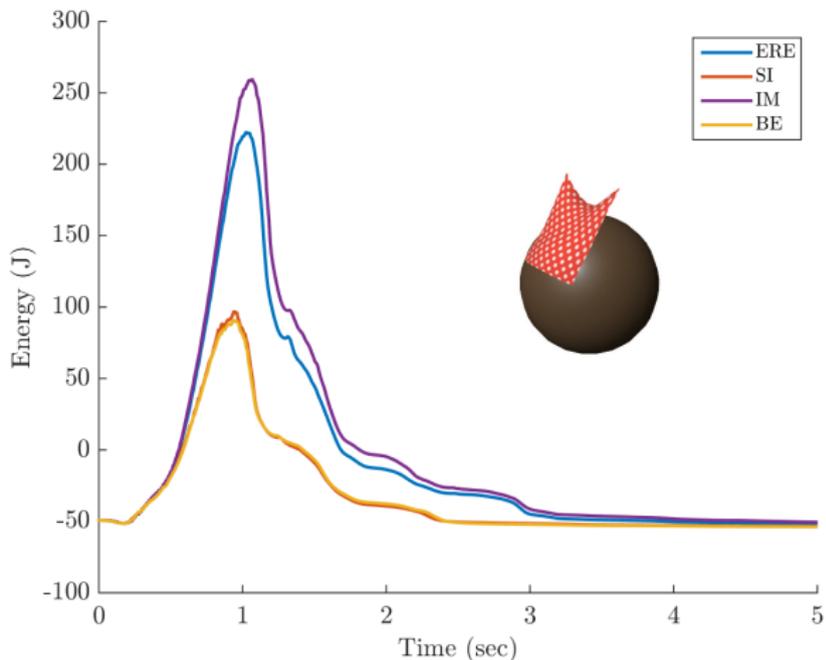
# FRICTION CONSTRAINT FORCE



# FRICTION CONSTRAINT FORCE

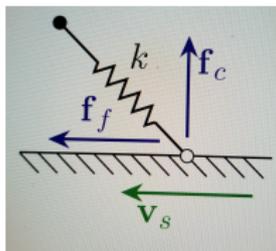


- ▶ Solution for Coulomb force is an inclusion which is difficult to handle and non-smooth
- ▶ Approximate it using a smoothed penalty model
- ▶ *Can't apply "optimization" approach*
- ▶ Instead of using a **lagged frictional contact** (which uses  $\mathbf{q}$  for evaluating friction force) use damped Newton for the **"fully implicit"** equations



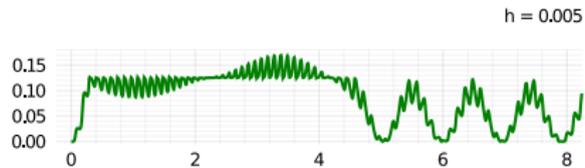
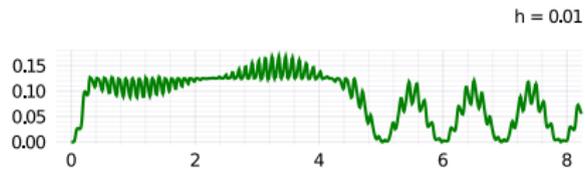
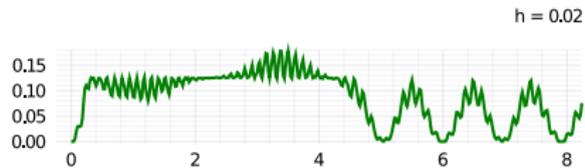
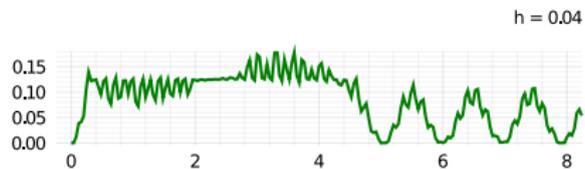
- ▶ With lagged friction might drop the bowl
- ▶ With lagged friction + TR might get instability
- ▶ Using inexact Newton
- ▶ Two real-world examples

# POSSIBLE INSTABILITIES?

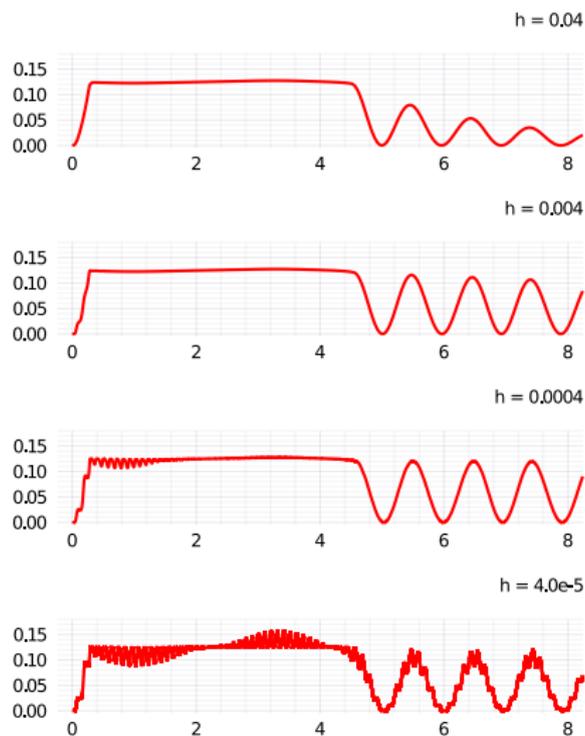


- ▶ Yes they can arise
- ▶ Fortunately they are local and overall stability not affected
- ▶ Less noticed for highly damping integrators, more for conservative ones
- ▶ Analysis in Larionov's thesis and our paper

# LOCAL INSTABILITY USING TR



# LOCAL INSTABILITY USING BE



TR-BDF2 is in between TR and BE

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[Boesen, Haber & Ascher '22]

# NEURAL ODE

- ▶ Statistical learning: given data pairs  $(\mathbf{x}_i, \mathbf{y}_i)$ ,  $i = 1, \dots, n$  find a function  $\mathbf{h}$  depending on parameters  $\boldsymbol{\theta}$  s.t.

$$\mathbf{h}(\mathbf{x}, \boldsymbol{\theta}) = \mathbf{y} \quad \mathbf{x} \in X, \mathbf{y} \in Y$$

Look at neural networks for  $\mathbf{h}$

- ▶ A **residual neural network** may be considered as a **simple** discretization of a **large** initial-value ODE system

$$\begin{aligned} \mathbf{u}(0) &= K_0 \mathbf{x} \\ \frac{d\mathbf{u}}{d\tau} &= \mathbf{f}(\mathbf{u}, \boldsymbol{\theta}) \quad 0 \leq \tau \leq 1 \\ \mathbf{y} &= K^1 \mathbf{u}(1) \end{aligned}$$

Next, suppose we also know  $\mathbf{c}$  such that  $\mathbf{c}(\mathbf{y}) = \mathbf{c}(K^1 \mathbf{u}(1)) = \mathbf{0}$

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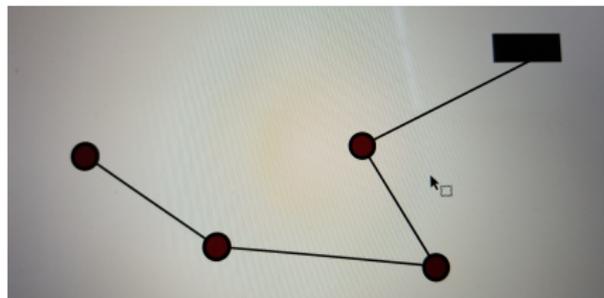
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# CONSTRAINED NEURAL ODE

- ▶ Suppose we also know  $\mathbf{c}$  such that  $\mathbf{c}(\mathbf{y}) = \mathbf{c}(K^o \mathbf{u}(1)) = \mathbf{0}$
- ▶ Can constrain  $K^o \mathbf{u}(\tau)$  in a lower dimensional physical space so

$$\mathbf{c}(K^o \mathbf{u}(\tau)) = \mathbf{0} \quad 0 \leq \tau \leq 1$$

- ▶ May want to constrain the residual neural network to better respect the physical constraint



## RESULTS SAMPLE

	Constraints	$n_t = 100$		$n_t = 1000$		$n_t = 10000$	
		MAE	CV	MAE	CV	MAE	CV
$k = 100$	No constraints	17.7	10.3	7.39	5.06	1.54	1.15
	Auxiliary loss $\eta = 3$	17.7	7.41	7.77	4.35	1.51	0.94
	Penalty $\gamma = 3$	17.5	9.65	7.01	3.99	1.63	0.96
	End con $\gamma, \eta = 3$	14.0	0.00	5.70	0.00	1.29	0.00
	Smooth con $\gamma, \eta = 3$	<b>11.2</b>	0.00	<b>3.35</b>	0.00	<b>1.02</b>	0.00
$k = 200$	No constraints	46.1	25.2	26.1	13.4	3.26	2.30
	Auxiliary loss $\eta = 1$	46.1	20.5	25.9	10.4	3.32	2.03
	Penalty $\gamma = 1$	45.5	24.2	25.9	13.1	3.42	2.34
	End con $\gamma, \eta = 1$	42.6	6.91	27.8	2.66	3.04	0.00
	Smooth con $\gamma, \eta = 1$	<b>33.3</b>	0.00	<b>19.1</b>	0.00	<b>2.21</b>	0.00

**TABLE:** Mean absolute error (MAE) and constraint violation (CV), in cm, over a test set of 1000 samples on the multi-body pendulum problem.  $n_t$  is the number of training samples, while  $k$  is the number of steps predicted ahead. Each experiment was repeated three times and the average of those runs are shown.

# NEURAL DAE

- ▶ A **residual neural network** may be considered as a **simple** discretization of a **large** initial-value ODE system
- ▶ Recall that a given DAE in the physical world can often be considered as an ODE with an algebraic invariant
- ▶ Ignoring the invariant we can construct a neural ODE also for a physical **semi-explicit DAE**
- ▶ Moreover *the traditional issue of drift off the constraint is possibly avoided because the NN is learned from solution examples independent of constraint differentiation*

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# CONCLUSIONS

- ▶ **Old** understanding of the nature of DAEs and of methods for handling them numerically has proved useful when facing new complex applications
- ▶ **New** perspectives had to be introduced to handle these new situations